

Advanced Pumping Systems

SYSTEM DESCRIPTION

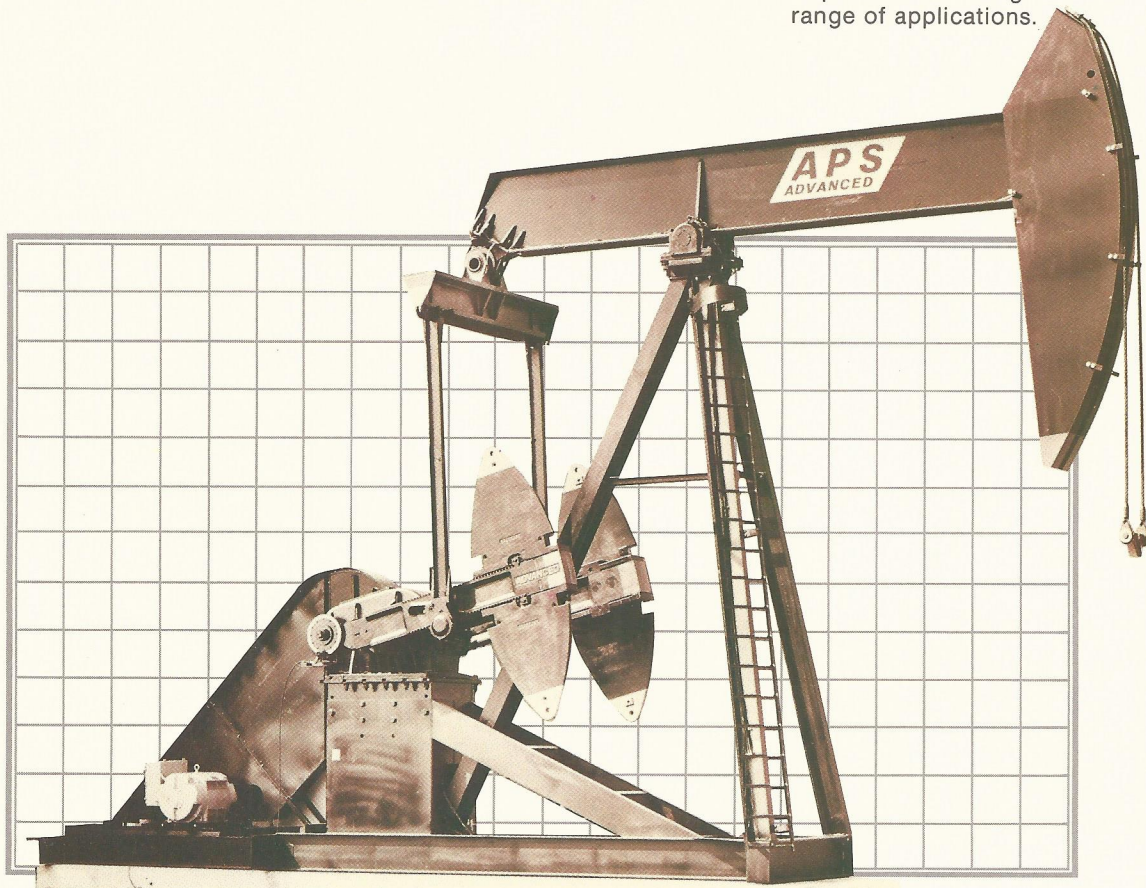
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The APS ADVANCED™ Universal Pumping System

The APS ADVANCED unit is the first universal crank-balanced pumping unit ever introduced.

Two APS ADVANCED universal structures handle a full range of requirements which previously required over 35 different API sized conventional units.

The APS ADVANCED universal units have been computer designed for absolute minimum gear reducer and prime mover requirements throughout the full range of applications.



Features:

- **UNIVERSAL DESIGN** — Two APS structures cover 114 through 912 applications.
- **GEAR REDUCER INTERCHANGEABILITY** — Each APS structure accommodates four interchangeable herringbone gear reducer sizes.
- **FULLY ADJUSTABLE STROKE** — Each APS structure allows continuous stroke adjustment over a range nearly double that of ordinary crank-balanced units.
- **OPTIMUM SYSTEM EFFICIENCY** — Each APS structure has a typical torque reduction of 35% compared to ordinary units.
- **LOWER SUCKER ROD STRESS** — The softer APS upstroke motion maximizes sucker rod life.
- **GEAR REDUCER LOAD REVERSALS MINIMIZED** — The smoother APS load curve results in longer reducer life, as load reversals have been essentially eliminated.
- **COUNTERBALANCING SIMPLE AND PRECISE** — Only one type of master and auxiliary weight is required for all 114 through 912 applications.
- **MINIMUM OPERATIONAL COSTS** — Energy savings can recover initial pumping unit investment within 3 years.
- **INVENTORY LOGISTICS MINIMAL** — The APS universal design reduces inventory requirements to an absolute minimum.
- **COMPETITIVE PRICE** — The APS universal design and commonality of tooling provide substantial overdesign at competitive prices.
- **COMPUTER SERVICE AVAILABLE** — Each customer application can be computer modeled by APS.
- **LABORATORY AND FIELD TESTING** — Complete structural performance can be verified on the state-of-the-art APS laboratory well simulator and the on-site systems analyzer.

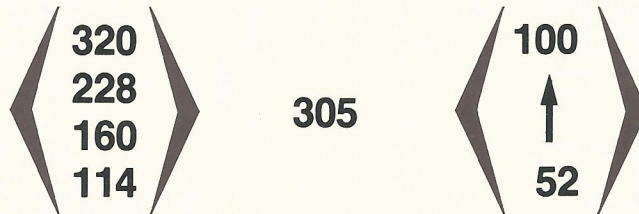
UNIT DESIGNATIONS

THE ADVANCED 365-168 UNIVERSAL PUMPING UNIT *



4 Interchangeable Gear Reducers; 36,500# Structural Capacity; Any Stroke from 88" to 168"

THE ADVANCED 305-100 UNIVERSAL PUMPING UNIT *



4 Interchangeable Gear Reducers; 30,500# Structural Capacity; Any Stroke from 52" to 100"

* Basic Structure Includes: T-base, universal prime mover base, universal belt guard, wireline and carrier bar, brake assembly, safety ladder, ground oiling system, oil in reducer, required gear reducer and reducer sheave. Counterbalance weights are separately ordered according to the enclosed counterbalance effect charts. Consult APS for wide bases, custom prime mover mounting interfaces, crank guards and other accessories.

GEAR REDUCER SPECIFICATIONS

Authorization  #3924

All reducers are double reduction herringbone and feature split housings with bearing carriers for maintenance serviceability. Gear reducers are manufactured to APS specifications by Curtis Machine Company of Dodge City, Kansas.

	Reducer Size	Peak Torque Rating	Maximum Sheave	Sheave Bore	Gear Ratio
APS MODEL 365-168	912	912,000 in-lb	58" P.D.	3.875"	30.412
	640	640,000 in-lb	58" P.D.	3.875"	30.412
	456	456,000 in-lb	44" P.D.	3.000"	29.975
	320	320,000 in-lb	44" P.D.	3.000"	29.975
APS MODEL 305-100	320	320,000 in-lb	44" P.D.	3.000"	29.975
	228	228,000 in-lb	36" P.D.	2.500"	29.816
	160	160,000 in-lb	36" P.D.	2.500"	29.816
	114	114,000 in-lb	36" P.D.	2.500"	29.816

COMPONENT DESCRIPTIONS

APS has applied for patents on the universal linkage, the universal crank assembly and several universal subsystem components.

All structural bearings are self-aligning spherical bearings. The saddle assembly and the horsehead are adjustable for simple alignment. The crank pin can be continuously adjusted along a vernier scale for **any** exact stroke length required within the range of each unit. The universal crank weights are easily adjusted and locked for **any** precise counterbalance effect required.

COUNTERBALANCE DATA

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APS MODEL 365-168

(PHASE ANGLE $\tau = -12.5^\circ$) COUNTERBALANCE EFFECT AT $\theta = 90^\circ$ CRANK ANGLE

WEIGHT COMPLEMENT*	TOTAL WEIGHT ADDED	MAXIMUM MOMENT, M (OCCURS AT $\theta = 102.5^\circ$)	NOTE: STRUCTURAL UNBALANCE IS ZERO FOR ALL STROKES																				
			88"	92"	96"	100"	104"	108"	112"	116"	120"	124"	128"	132"	136"	140"	144"	148"	152"	156"	160"	164"	168"
Cranks Only	0	283460	6675	6399	6146	5915	5701	5505	5323	5154	4997	4851	4715	4588	4469	4358	4254	4157	4065	3980	3899	3824	3753
2MW	2000	440960 - (2000 x ΔR)	10384	9955	9562	9201	8870	8563	8280	8018	7774	7547	7335	7138	6953	6780	6619	6467	6325	6191	6066	5949	5839
4MW	4000	598460 - (4000 x ΔR)	14094	13510	12977	12488	12038	11622	11238	10882	10551	10243	9955	9687	9437	9202	8983	8777	8584	8403	8233	8074	7925
4MW + 2A	6000	755960 - (6000 x ΔR)	17803	17066	16392	15775	15206	14681	14196	13746	13328	12938	12576	12237	11920	11624	11347	11087	10843	10615	10400	10199	10011
4MW + 4A	8000	913460 - (8000 x ΔR)	21512	20622	19808	19061	18374	17740	17153	16610	16104	15634	15196	14786	14404	14046	13711	13397	13102	12826	12567	12324	12096
4MW + 6A	10000	1070960 - (10000 x ΔR)	25221	24177	23223	22348	21542	20799	20111	19473	18881	18330	17816	17336	16888	16466	16075	15707	15362	15038	14734	14449	14182
4MW + 8A	12000	1228460 - (12000 x ΔR)	28931	27733	26639	25635	24710	23857	23069	22337	21658	21026	20436	19886	19371	18890	18439	18017	17621	17249	16901	16574	16268
4MW + 10A	14000	1385960 - (14000 x ΔR)		31289	30054	28921	27879	26916	26026	25201	24435	23721	23056	22435	21855	21312	20804	20327	19880	19461	19066	18694	18354
4MW + 12A	16000	1543460 - (16000 x ΔR)				32208	31047	29975	28984	28065	27212	26417	25676	24985	24338	23734	23168	22637	22139	21673	21235	20824	20440
4MW + 12A + 2AA	18000	1700960 - (18000 x ΔR)							31942	30929	29989	29113	28296	27534	26822	26156	25532	24947	24398	23884	23402	22949	22525
4MW + 12A + 4AA	20000	1858460 - (20000 x ΔR)										31808	30917	30084	29306	28578	27896	27257	26658	26096	25568	25074	24611
4MW + 12A + 6AA	22000	2015960 - (22000 x ΔR)													31789	31000	30260	29566	28917	28307	27735	27199	26697
4MW + 12A + 8AA	24000	2173460 - (24000 x ΔR)															31876	31176	30519	29902	29324	28783	

$$T_n = (W \times TF) - M \sin(\theta - 12.5^\circ) \text{ in-lb}$$

- T_n = instantaneous net required reducer torque at crankshaft at any crank angle θ (usually in 15° increments)
- W = instantaneous well load at crank angle θ determined by dynamometer readings — after translating position of rod, POR, to crank angle θ per POR charts (usually in 15° increments)
- θ = instantaneous crank angle defining the clockwise angular position of the line between crankshaft and crank pin from its 12 o'clock spatial position
- τ = -12.5° which means that the crank weight and its weight complement have a composite center of gravity which trails crank angle θ by 12.5° with crankshaft rotating clockwise
- TF = torque factor describing number of in-lb of torque at crankshaft per 1 lb. of well load at any instantaneous crank angle θ at any stroke setting per TF charts (usually in 15° increments)
- M = maximum moment of crank weight and its weight complement at crankshaft for any radially adjusted position of the weight complement (occurs at $\theta = 102.5^\circ$ crank angle)
- ΔR = distance that weight complement is adjusted radially inward from the fully outboard position

$$M \left\{ \begin{array}{l} \bullet \text{ obtained directly from above chart for any } \Delta R \\ \text{or} \\ \bullet \text{ } M = 1.0243 \times 90^\circ \text{CBE} \times 90^\circ \text{TF} \text{ in-lb} \end{array} \right.$$

90°CBE = exact counterbalance effect at polished rod at $\theta = 90^\circ$ crank angle for any weight complement, for any stroke setting and for any ΔR inward adjustment of weight complement

$$90^\circ \text{CBE} = 90^\circ \text{CBE}_s - \frac{\Delta R}{78.75} \times (90^\circ \text{CBE}_s - 90^\circ \text{CBE}_{\text{sco}}) \text{ lbs}$$

90°CBE_s = counterbalance effect off chart for any fully-outboard weight complement and for any stroke, including interpolated values for any stroke in between those listed

$90^\circ \text{CBE}_{\text{sco}}$ = counterbalance effect off chart for cranks only configuration, including interpolated values for any stroke in between those listed

Note: Exact 90°CBE can also be measured in the field by disconnecting the well load and measuring force required at carrier bar for linkage equilibrium at crank angle $\theta = 90^\circ$

* Crank accommodates 4 master weights (4MW) each weighing 1000# and has auxiliary weights available (A) each weighing 1000# and other auxiliary weights (AA) each weighing 1000# — with (AA) auxiliaries only to be used if total required weight complement exceeds 4MW+12A

- Notes:
1. APS units should only be operated in clockwise direction as defined with polished rod to the right.
 2. When having to adjust weight complement radially inward, it is necessary to adjust each of the 4 weight sub-complements radially inward the same amount as measured from the outboard end of each crank.
 3. In certain special cases, the weight sub-complements can be configured to modify the phase angle τ if desired (consult APS).
 4. Counterbalance effect interpolation can be completely avoided if operation is at any of the exact strokes in the charts, which are listed in $4''$ increments.

COUNTERBALANCE DATA

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APS MODEL 305-100

COUNTERBALANCE EFFECT AT $\theta = 90^\circ$ CRANK ANGLE

(PHASE ANGLE $\tau = -15.75^\circ$)

WEIGHT COMPLEMENT*	TOTAL WEIGHT ADDED	MAXIMUM MOMENT, M (OCCURS AT $\theta = 105.75^\circ$)	NOTE: STRUCTURAL UNBALANCE IS ZERO FOR ALL STROKES												
			52"	56"	60"	64"	68"	72"	76"	80"	84"	88"	92"	96"	100"
CRANKS ONLY	0	106610	4271	3979	3727	3507	3314	3143	2991	2855	2734	2624	2526	2436	2356
2MW	2000	205610 - (2000 x ΔR)	8237	7674	7188	6764	6391	6062	5769	5508	5273	5062	4871	4699	4543
4MW	4000	304610 - (4000 x ΔR)	12204	11369	10649	10021	9469	8981	8547	8160	7812	7499	7217	6962	6731
4MW + 2A	6000	403610 - (6000 x ΔR)	16170	15065	14110	13278	12547	11900	11325	10812	10351	9937	9563	9225	8919
4MW + 4A	8000	502610 - (8000 x ΔR)	20136	18760	17571	16534	15624	14819	14103	13464	12890	12374	11909	11488	11107
4MW + 6A	10000	601610 - (10000 x ΔR)	24103	22455	21032	19791	18702	17738	16881	16116	15429	14812	14254	13750	13295
4MW + 8A	12000	700610 - (12000 x ΔR)		26150	24493	23048	21779	20657	19659	18768	17968	17249	16600	16013	15483
4MW + 10A	14000	799610 - (14000 x ΔR)				26305	24857	23576	22438	21420	20507	19687	18946	18276	17670
4MW + 12A	16000	898610 - (16000 x ΔR)						26495	25216	24072	23046	22124	21292	20539	19858
4MW + 12A + 2AA	18000	997610 - (18000 x ΔR)								26724	25586	24562	23637	22802	22046
4MW + 12A + 4AA	20000	1096610 - (20000 x ΔR)										26999	25983	25065	24234

$$T_n = (W \times TF) - M \sin(\theta - 15.75^\circ) \text{ in-lb}$$

T_n = instantaneous net required reducer torque at crankshaft at any crank angle θ (usually in 15° increments)

W = instantaneous well load at crank angle θ determined by dynamometer readings — after translating position of rod, POR, to crank angle θ per POR charts (usually in 15° increments)

θ = instantaneous crank angle defining the clockwise angular position of the line between crankshaft and crank pin from its 12 o'clock spatial position

τ = -15.75° which means that the crank weight and its weight complement have a composite center of gravity which trails crank angle θ by 15.75° with crankshaft rotating clockwise

TF = torque factor describing number of in-lb of torque at crankshaft per 1 lb. of well load at any instantaneous crank angle θ at any stroke setting per TF charts (usually in 15° increments)

M = maximum moment of crank weight and its weight complement at crankshaft for any radially adjusted position of the weight complement (occurs at $\theta = 105.75^\circ$ crank angle)

ΔR = distance that weight complement is adjusted radially inward from the fully outboard position

$$M \left\{ \begin{array}{l} \bullet \text{ obtained directly from above chart for any } \Delta R \\ \text{or} \\ \bullet \text{ } M = 1.0390 \times 90^\circ \text{CBE} \times 90^\circ \text{TF} \text{ in-lb} \end{array} \right.$$

90°CBE = exact counterbalance effect at polished rod at $\theta=90^\circ$ crank angle for any weight complement, for any stroke setting and for any ΔR inward adjustment of weight complement

$$90^\circ \text{CBE} = 90^\circ \text{CBE}_s - \frac{\Delta R}{49.5} \times (90^\circ \text{CBE}_s - 90^\circ \text{CBE}_{\text{SCO}}) \text{ lbs}$$

90°CBE_s = counterbalance effect off chart for any fully-outboard weight complement and for any stroke, including interpolated values for any stroke in between those listed

$90^\circ \text{CBE}_{\text{SCO}}$ = counterbalance effect off chart for cranks only configuration, including interpolated values for any stroke in between those listed

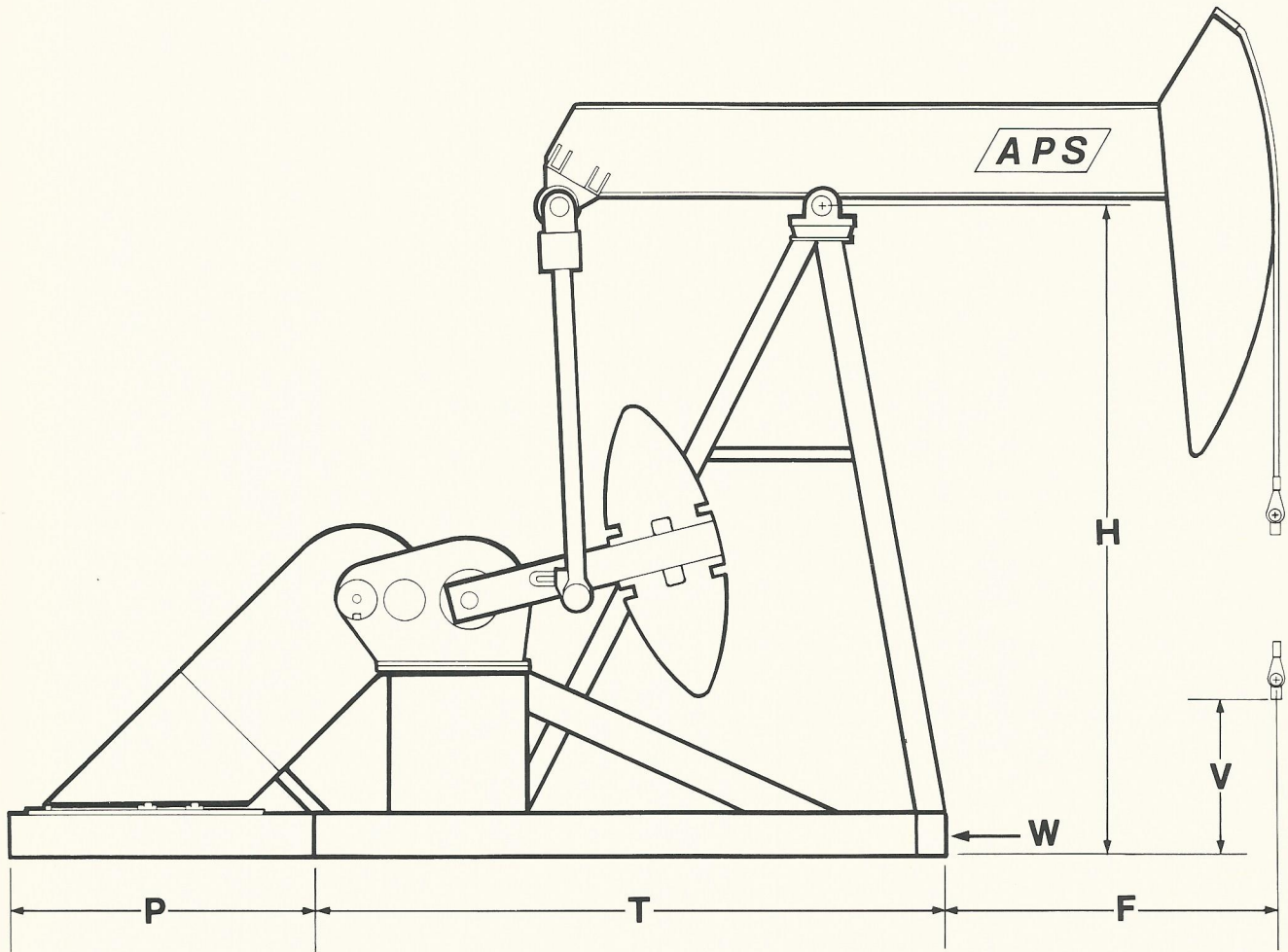
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UNIT DIMENSIONS

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	F	H	P	T	V	W
APS MODEL 365-168	133.56"	260.12"	122.00"	251.87"	63.12"	81.50"
APS MODEL 305-100	92.25"	201.83"	122.00"	206.75"	63.12"	65.50"

WARRANTY

In accordance with the standard APS warranty, APS warrants its pumping units against defective material and workmanship for a period of eighteen (18) months after installation or twenty-four (24) months after shipment from factory — whichever occurs first.

Advanced Pumping Systems, Inc. manufactures the new ADVANCED universal pumping unit, related systems and state-of-the-art oil well simulation and analysis equipment.

APS was formed by a group of oil production systems specialists and aerospace design engineers who combined oil industry production expertise with advanced technological engineering to achieve a major breakthrough in pumping technology.

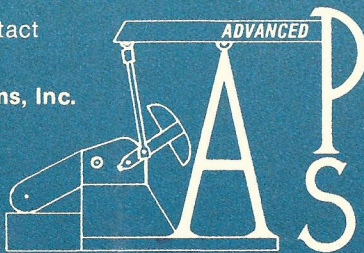
Patents are pending on many design features.

APS equipment surpasses the present competition due to its superior performance, cost effectiveness, operational simplicity and complete versatility.

For more information, contact
the Sales Department.

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Patents Pending